



Influence of chemical composition and structural factors of $\text{Fe}_2\text{O}_3/\text{In}_2\text{O}_3$ sensors on their selectivity and sensitivity to ethanol[☆]

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Received 20 April 2003; received in revised form 10 July 2003; accepted 17 July 2003

Abstract

The influence of structure, phase composition, system dispersity and particle morphology of Fe_2O_3 - and In_2O_3 -based thin film layers on the electrical parameters of the corresponding gas sensors was studied in this paper. High selectivity and sensitivity of heterostructural $\gamma\text{-Fe}_2\text{O}_3/\text{In}_2\text{O}_3$ thin film sensors in the detection of alcohols has been here established. As it was found, the above mentioned sensors are almost insensitive to NO_2 , O_3 , CO and CH_4 at the operating temperature which is optimal for alcohol detection (300°C). The peculiarities of sensor behaviour are discussed taking into account the activity of Fe_2O_3 layers in the reductive-oxidative and acid-base processes accompanying the adsorption of CH_3OH and $\text{C}_2\text{H}_5\text{OH}$ molecules at the oxide surface.

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Keywords: Gas sensor; Oxide heterojunction; $\text{Fe}_2\text{O}_3/\text{In}_2\text{O}_3$; Alcohol; Selectivity

1. Introduction

Iron oxides are known to be widely used materials as active element of ceramic and thick film gas sensors, but there are only few items of information concerning the application of iron oxide as thin film sensing layers. This paper is mainly aimed at the determination of the influence of some structural features of $\text{Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ films on their gas-sensitive properties. Great attention was paid to heterojunction structure $\text{Fe}_2\text{O}_3\text{-In}_2\text{O}_3/\text{In}_2\text{O}_3$, which is found to be advanced material for reducing gas detection.

From the available references, it follows that the sensitivity of ceramic sensors based on Fe_2O_3 towards reducing gases is rather low [1–3]. However, doping of Fe_2O_3 with quadrivalent metal ions (Sn, Ti, Zr), as well as modifying of a sensitive material with SO_4^{2-} ions, can significantly enhance the gas-sensitive properties of the corresponding sensors regarding ethanol and hydrocarbons [3], addition of Fe_2O_3 to SnO_2 leads to an improved response of thick films towards ethanol [4]. There are also some items of literature concerning the effect of Fe_2O_3 additives on the properties of In_2O_3 based sensors. $\text{MoO}_3\text{-SnO}_2$ sensors are known to be

extremely selective regarding ethanol [5] and may serve as reference point when detection of alcohol is considered. It is known that the doping of SnO_2 and In_2O_3 with $\gamma\text{-Fe}_2\text{O}_3$ increases their sensitivity to oxidising gases (O_3 , NO_2) [6]. But there are only little references regarding $\gamma\text{-Fe}_2\text{O}_3$ using as thin film sensors towards reducing gases. And the data available are not sufficient in order to realize full picture of iron-containing material application in gas sensor industry.

2. Experimental

Gas-sensitive properties of thin film sensors containing one oxide layer (Fe_2O_3 , In_2O_3) and bi-layers ($\text{Fe}_2\text{O}_3/\text{In}_2\text{O}_3$, $\text{Fe}_2\text{O}_3\text{-In}_2\text{O}_3/\text{In}_2\text{O}_3$) have been investigated here. Sensor response values to CH_3OH , $\text{C}_2\text{H}_5\text{OH}$ (100–500 ppm), CH_4 , CO (50 ppm) were estimated.

The sensitive elements were formed from the stabilised sols of the corresponding metal hydroxides that were obtained by sol-gel technique. The procedure of sol preparation used in this study consisted in the following steps: (i) forced hydrolysis of inorganic metal salt solution (FeCl_2 , $\text{Fe}(\text{NO}_3)_3$, $\text{In}(\text{NO}_3)_3$) with base agent (NH_3); (ii) precipitation of metal hydroxide followed by its separation; (iii) formation of sol through peptization of the deposit with peptizing agent or as a result of self-peptization. Methods of $\text{Fe}_2\text{O}_3 \cdot n\text{H}_2\text{O}$ sol synthesis providing the formation of both

[☆] Presented at Eurosensors XVI Prague, 2002.

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64 γ -Fe₂O₃ and α -Fe₂O₃ oxides under heating were used; be-
 65 sides, two types of γ -Fe₂O₃ layers (prepared via Fe(OH)₂
 66 as an intermediate (I- γ -Fe₂O₃) and via Fe₃O₄ (II- γ -Fe₂O₃)
 67 sols) were here studied. The composites were prepared by
 68 both combined Fe(OH)₂ and In(OH)₃ hydroxide precipita-
 69 tion followed by their oxidation with oxygen (a flow of air
 70 was passed through the suspension during 5–6 h at 30 °C)
 71 and by mixing of individual sols of Fe₂O₃ and In(OH)₃ in
 72 required proportions.

73 To form thin film layers, sols were deposited onto poly-
 74 crystalline Al₂O₃ substrates (3 mm × 3 mm × 0.25 mm) sup-
 75 plied with Pt interdigital electrode structure on the front
 76 side and Pt meander heater on the backside. An In₂O₃
 77 sub-layer was preliminary deposited onto the substrate in
 78 order to knowingly form heterojunction structure and pro-
 79 vide suitable sensor electroconductivity. For comparison,
 80 single-layer sensors, consisting of only In₂O₃ or Fe₂O₃ have
 81 also been studied. The samples were dried at 25 °C followed
 82 by annealing at 300 °C in air. The sensor response was cal-
 83 culated as $S = \Delta G/G_{\text{air}}$, where G and G_{air} is the conduc-
 84 tivity of sensitive layer in alcohol–synthetic air mixture and
 85 in synthetic air consequently (RH 30%).

86 The structure of the simple oxides (Fe₂O₃, In₂O₃) and
 87 nanocomposites (Fe₂O₃–In₂O₃) has been characterised by
 88 means of X-ray diffraction (HZG-4A diffractometer, Co K α
 89 radiation, Ni-filter, angle range 20–70°).

90 3. Results and discussion

91 The variation of electrical conductivity, system dispersity
 92 and oxide particle sintering of both simple oxides (Fe₂O₃,
 93 In₂O₃) and Fe₂O₃–In₂O₃ composites as a function of the
 94 synthesis conditions, components ratio and operating tem-
 95 perature was analysed in the paper.

96 Fig. 1 clearly illustrates the fact that the sensors based
 97 on single Fe₂O₃ and In₂O₃ layers have practically the same

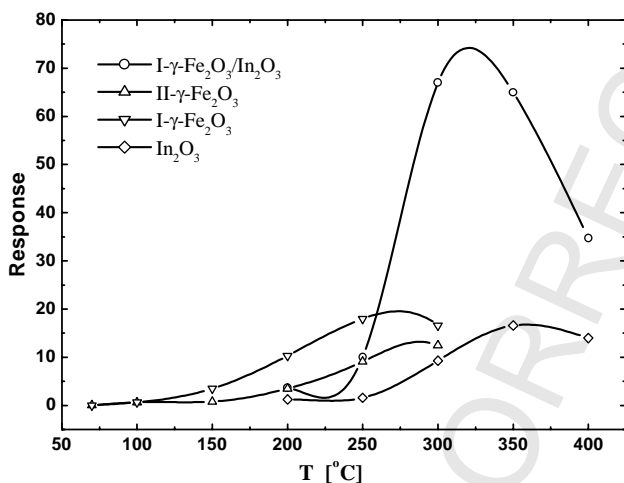


Fig. 1. Temperature-dependent response of In₂O₃ and Fe₂O₃ thin film sensors to C₂H₅OH (100 ppm, RH 30%).

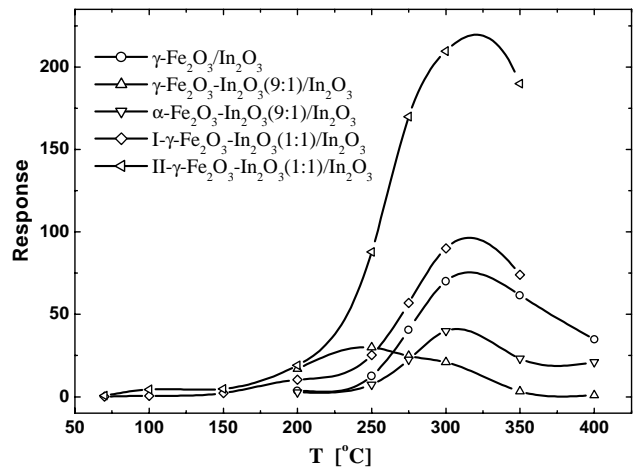


Fig. 2. Temperature-dependent response of In₂O₃–Fe₂O₃ bi-layer thin film sensors to C₂H₅OH (100 ppm, RH 30%).

98 response values to ethanol, but they slightly differ regard-
 99 ing the optimal operating temperature. The sensors based on
 100 γ -Fe₂O₃/In₂O₃ heterostructure (bi-layer sensors) are char-
 101 acterised by significantly higher sensitivity to ethanol than
 102 the single-layer (γ -Fe₂O₃, In₂O₃) ones. In this case, In₂O₃
 103 sub-layer not only provides the sufficient γ -Fe₂O₃/In₂O₃
 104 film conductivity, but it has a clear influence on the sensor
 105 sensitivity. We suppose that the important point influencing
 106 strongly the activity of sensor is the presence of phase in-
 107 terface in such a sample. Note, that both In₂O₃ and Fe₂O₃
 108 layers demonstrates typical semiconducting behaviour [7].

109 The addition of In₂O₃ (10 mol%) to γ -Fe₂O₃ layer
 110 leads to decreasing of the γ -Fe₂O₃/In₂O₃ sensor re-
 111 sponse to ethanol (Fig. 2). According to the XRD data,
 112 γ -Fe₂O₃–In₂O₃ (9:1) composite has the structure of In³⁺
 113 in γ -Fe₂O₃ lattice solid solution (Fig. 3); certain amount
 114 of C–In₂O₃ phase is also presented. On the contrary, fur-
 115 ther increasing of In₂O₃ content within γ -Fe₂O₃ layer of
 116 γ -Fe₂O₃/In₂O₃ structure up to 50 mol% causes abrupt rising
 117 of its sensitivity, which even overwhelms the sensitivity of
 118 γ -Fe₂O₃/In₂O₃ sample. In comparison with γ -Fe₂O₃–In₂O₃
 119 (9:1) sample, γ -Fe₂O₃–In₂O₃ (1:1) one probably consists
 120 of two highly dispersive phases (see Fig. 3) with great phase
 121 interface. From the XRD data of the sample it is difficult to
 122 determine exactly phase composition of the sample because
 123 of the similarity of γ -Fe₂O₃ and C–In₂O₃ crystal lattices.
 124 The growth of γ -Fe₂O₃–In₂O₃ (1:1) dense layer is due to the
 125 formation of numerous bonds between the oxide particles
 126 within this composite. Both developed surface of contacting
 127 oxides and their specific morphology results in significant
 128 improvement of γ -Fe₂O₃–In₂O₃ sensitive species.

129 Moreover, Fe₂O₃–In₂O₃/In₂O₃ sensor sensitivity hardly
 130 depends on the crystal structure of the active layers, in par-
 131 ticular, Fe₂O₃ phase. There are two possible Fe₂O₃ phases,
 132 suitable under operating temperatures used γ -Fe₂O₃ and
 133 α -Fe₂O₃. In the case of the pure γ -Fe₂O₃, the response
 134 achieves its maximum value at lower temperatures (250 °C)

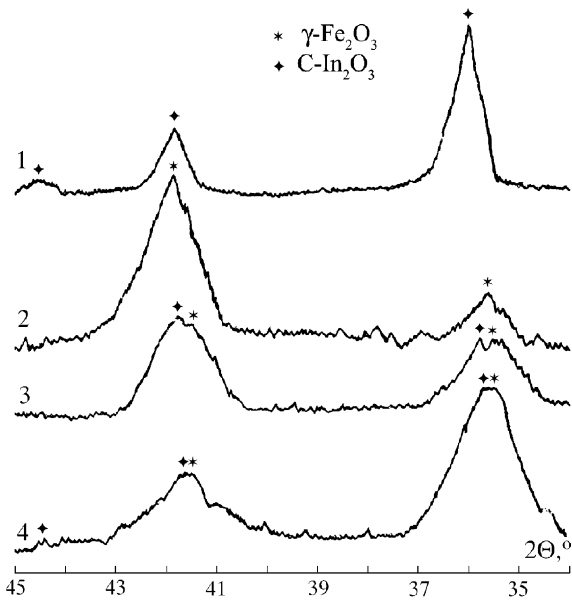


Fig. 3. XRD patterns of In_2O_3 , $\gamma\text{-Fe}_2\text{O}_3$ and $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ composites annealed at 300°C (1 h): (1) In_2O_3 ; (2) $\gamma\text{-Fe}_2\text{O}_3$; (3) $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (9:1); (4) $\gamma\text{-In}_2\text{O}_3\text{-Fe}_2\text{O}_3$ (1:1).

135 than in the case of $\alpha\text{-Fe}_2\text{O}_3$ (300°C). Higher activity of
 136 $\gamma\text{-Fe}_2\text{O}_3$ phase is associated with specificity of its structure:
 137 the presence of metal cation vacancies within crystalline lattice
 138 and the readiness of $\text{Fe}^{2+} \leftrightarrow \text{Fe}^{3+}$ transformation under
 139 the exposure of gas media. Besides, partial reversible
 140 reduction of $\gamma\text{-Fe}_2\text{O}_3$ layer to form $\alpha\text{-Fe}_2\text{O}_3$ is possible.
 141 The product of reduction is highly dispersive and strongly
 142 reactive and resembles the behaviour of γ -phase of Fe_2O_3 .
 143 When methanol detection is considered, one can observe the
 144 same regularities inherited to ethanol, excepting the lower
 145 response (Fig. 4).

146 The conditions of $\gamma\text{-Fe}_2\text{O}_3$ sol preparation influence also
 147 the $\gamma\text{-Fe}_2\text{O}_3$ phase microstructure and the sensor activity
 148 (Table 1).

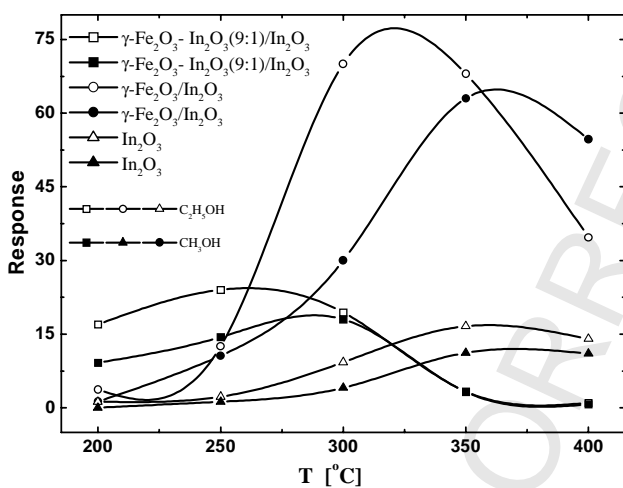


Fig. 4. Comparison of In_2O_3 and Fe_2O_3 based thin film sensor behaviour in $\text{C}_2\text{H}_5\text{OH}$ and CH_3OH media (100 ppm, RH 30%).

Table 1

The response of thin film sensors of various compositions to ethanol and CO

Sensor	dG/G CO (50 ppm)	T (°C)	dG/G EtOH (100 ppm)	T (°C)
In_2O_3	0.45	350	15	350
$\alpha\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (9:1)/ In_2O_3	0.9	300	45	300
I- $\gamma\text{-Fe}_2\text{O}_3$ / In_2O_3	1.25	350	65	300
I- $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (9:1)/ In_2O_3	0.9	250	25	250
I- $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (1:1)/ In_2O_3	0.8	250	125	300
II- $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (1:1)/ In_2O_3	0.1	350	200	300
I- $\gamma\text{-Fe}_2\text{O}_3$	-0.9	150	12	250
II- $\gamma\text{-Fe}_2\text{O}_3$	0.1	250	17	300

The layers having $\gamma\text{-Fe}_2\text{O}_3$ crystal structure show different particle sizes; it depends on the method of sol synthesis. $\gamma\text{-Fe}_2\text{O}_3$ films prepared by oxidation of $\text{Fe}(\text{OH})_2$ with molecular oxygen (method I) are highly dispersive (~ 5 nm), while II- $\gamma\text{-Fe}_2\text{O}_3$ sample synthesised by oxidation of Fe_3O_4 sol with oxygen is consisted of spherical particles of greater dimension (~ 20 nm) and of less developed phase interface. As a result, sensor based on simple I- $\gamma\text{-Fe}_2\text{O}_3$ demonstrates higher response than II- $\gamma\text{-Fe}_2\text{O}_3$ one (see Fig. 1). But in the case of $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ composites, prepared by $\gamma\text{-Fe}_2\text{O}_3$ and $\text{In}(\text{OH})_3$ sol mixing this regularity has reverse direction (see Fig. 2). The explanation follows from the comparison of the two simple oxide dispersity: the less grain size of an oxide the more homogeneous system one can get under sol mixing followed by the obtained powder thermal treatment. Thus, greater dimension of II- $\gamma\text{-Fe}_2\text{O}_3$ phase particles favours the formation of less homogeneous and, consequently, more active layers than in case of I- $\gamma\text{-Fe}_2\text{O}_3$.

Both $\gamma\text{-Fe}_2\text{O}_3/\text{In}_2\text{O}_3$ and $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3/\text{In}_2\text{O}_3$ sensors were found to be selective regarding alcohol vapours. These sensors are practically insensitive to CO, CH_4 , NO_2 and O_3 at the temperature which is optimal for ethanol detection (300°C). Table 2 shows that both $\gamma\text{-Fe}_2\text{O}_3/\text{In}_2\text{O}_3$ and $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (1:1)/ In_2O_3 thin film sensors are essentially more sensitive than $\text{SnO}_2\text{-MoO}_3$ samples which demonstrate high sensitivity to ethanol.

Dynamical parameters of the studied sensors are found to be suitable for thin film layers. Both response and recovery times lay in the range of 50–60 s at optimal operating temperatures (100 ppm $\text{C}_2\text{H}_5\text{OH}$, $300\text{--}350^\circ\text{C}$, RH 30%).

As it was noted earlier, the systems consisting of two contacting phases, In_2O_3 and $\gamma\text{-Fe}_2\text{O}_3$ are extremely sensitive to ethanol. In the case of $\gamma\text{-Fe}_2\text{O}_3\text{-In}_2\text{O}_3$ (1:1) com-

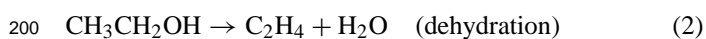
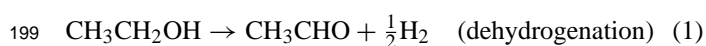
Table 2

The response of thin film sensors based on various oxides to ethanol (500 ppm) comparison

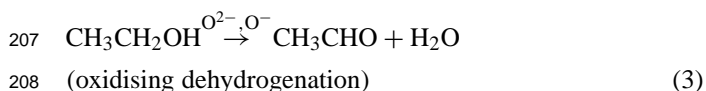
Sensor	dG/G	T (°C)
In_2O_3	15	350
$\gamma\text{-Fe}_2\text{O}_3/\text{In}_2\text{O}_3$	165	300
SnO_2	30	400
$\text{SnO}_2\text{-MoO}_3$	80	300

182 posite, grain size is less and surface of phase interface is
 183 greater (and, consequently, response values are greater) than
 184 those, typical for γ -Fe₂O₃/In₂O₃ heterocontact. The pres-
 185 ence of two phases within composite favours to the effec-
 186 tive course of multi-step process of both reductive–oxidative
 187 and acid–base interactions. Thus, alcohol detection is con-
 188 sidered as a process involving the two interactions between
 189 the detected molecules and the particles of the oxide ele-
 190 ment [2]. The obtained results concerning Fe₂O₃–In₂O₃ and
 191 SnO₂–MoO₃ based sensor were here interpreted assuming
 192 a different activity of the above systems in both processes.
 193 The possibility of intermediate further oxidation, the second
 194 phase take part in, is considerably increases sensor response
 195 values to ethanol.

196 Two ways of alcohol (for example, ethanol) molecule con-
 197 version are possible at oxide surface, dehydrogenation (1)
 198 and dehydration (2) [8–10].



201 Besides, further oxidation of the formed products (fore-
 202 most, oxidation of H atoms) is possible at oxide surface; it
 203 should result in sensor response growth. Thus, the process
 204 (1) most often proceeds through the oxidising dehydrogena-
 206 tion mechanism



209 As we established earlier [11], in the indicated process
 210 lattice oxygen is only participating at high operating temper-
 211 atures (300–400 °C). The role of adsorbed oxygen consists
 212 in regenerating of partially reduced oxide surface. The oxi-
 213 dising dehydrogenation of alcohol (3) is heterolytic catalytic
 214 reaction. The process involves both reductive–oxidative and
 215 acid–base steps [12]. In particular, alcohol molecule adsorp-
 216 tion at metal cation, which plays role of Lewis centre, is
 217 related to acid–base reaction. The relative measure of oxide
 218 activity in the oxidation reactions can be oxygen-oxide sur-
 219 face bonding energy. In fact, the less the energy of oxygen
 220 atom isolation from an oxide surface the higher the oxide
 221 oxidising ability. The reactivity of oxides in acid–base reac-
 222 tions depends on the electronegativity of cations M^{n+} .

$$223 \chi = \chi_0(2n + 1) \quad (4)$$

224 where χ_0 is the Pauling's electronegativity and n the ion
 225 charge. The electronegativity can be used as the measure of
 226 Lewis acid site activity. The adsorption of alcohol molecules
 227 at Lewis sites is going with great output. Complete oxidation
 228 of intermediate products is possible at the surface of the ox-
 229 ide, which is characterised by small values of M–O binding
 230 energy and electronegativity. According to the electroneg-
 231 ativity (χ) increasing the studied oxides can be placed as
 232 follows: In₂O₃ < Fe₂O₃ < SnO₂ < MoO₃ (Table 3) [13].

Table 3

The metal–oxygen binding energy for some oxides

Metal oxide	E_{M-O} (kcal/g per atom)	Electronegativity
MoO ₃	91	30.55
SnO ₂	70	17.64
Fe ₂ O ₃	56	13.72
In ₂ O ₃	–	12.46

233 But in the general case, reductive–oxidative and acid–base
 234 properties of oxide surface may not correlate.

235 Thus, detection of ethanol using oxide materials, where
 236 metal is greatly electronegative (MoO₃) is not accompanying
 237 by complete oxidation of intermediates, but is characterised
 238 by striking selectivity. In the range of considerable M–O
 239 bonding energy values, donor–acceptor interaction between
 240 alcohol molecules and $M^{m+}O^{2-}$ species become clearly ap-
 241 parent. Oxides, containing Mo(VI) cations, which are strong
 242 Lewis acids, are very active. In fact, the low bonding energy
 243 and strongly basic properties of an oxide promote further
 244 oxidation of intermediates of alcohol molecule transforma-
 245 tion (Fig. 5), thereby, increasing the corresponding sensor
 246 response values.

247 The oxides, which are characterised by the possibility
 248 of metal ion reduction without oxide phase state modifica-
 249 tion, have the greatest ability to promote oxidising dehy-
 250 drogenation processes. For instance, such oxides as MoO₃,
 251 In₂O₃ and Fe₂O₃ are inclined to facile the changing of metal
 252 ion oxidising state: Mo(VI) \leftrightarrow Mo(V), In(III) \leftrightarrow In(II),
 253 Fe(III) \leftrightarrow Fe(II), while oxide phase remains original.

254 The sensors based on heterojunction oxide show consid-
 255 erable response to alcohol (ethanol, methanol) vapours. The
 256 heterojunction between an oxide and solid solution phases
 257 appears to be very active in both adsorption and oxidation
 258 of alcohol. The presence of two types of centres possessing
 259 different reductive–oxidative and acid–base properties, and
 260 participating in the processes of the alcohol molecule trans-
 261 formation is essential requirement to achieve high sensor re-
 262 sponse when alcohol detection is considered. The centres of
 263 one type can suitably participate in adsorption–desorption
 264 processes of alcohol molecules, whereas complete oxidation
 265 of intermediates is effectively going at the centres of another
 266 type.

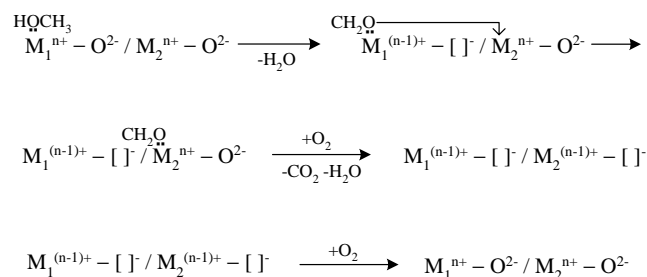


Fig. 5. The scheme of alcohol oxidation process at oxide phase interface by the example of methanol (CH₃OH) molecule oxidation.

The experimental data regarding both catalytic and gas-sensitive properties of most of semiconducting oxides are not in accord with prevailing conception, asserting that the alcohol detection is predominantly realised as dehydration process (2), when oxide with acidic properties are used, and as dehydrogenation (1) at base oxide surface [9]. Thus, MoO_3 possesses strong acidic behaviour. At the same time, it is one of the most efficient catalysts of methanol conversion into formaldehyde (reaction of dehydrogenation) [14]. By reason of MoO_3 high catalytic activity, it being added to SnO_2 species evokes the increasing the corresponding sensor sensitivity towards alcohols [10]. However, in this case, after-oxidation of formaldehyde, generated during dehydrogenation step, to form CO_2 and H_2O is impossible because of great Mo–O bond strength within MoO_3 . Using this fact one can explain lesser response of SnO_2 – MoO_3 sensors to ethanol in comparison with Fe_2O_3 – In_2O_3 ones.

The analysis of the literature available regarding catalytic alcohol decomposition allows us to conclude that the prevailing in gas sensor industry oxides are more active in dehydrogenation reactions rather than in dehydration. Relying on numerous experimental data, in [12] have been calculated the values of catalytic reactivity ($\ln K$) for different oxides in both dehydrogenation and dehydration of isopropyl alcohol at the same conditions of catalysis. Table 4 represents the values of catalytic reactivity for the oxides used in this paper.

It is important to note, the regularities obtained for isopropyl alcohol are proper for ethanol as well. However, there are no valid experimental data in the literature, allowing us to realise the detailed calculation of catalytic properties of the oxides regarding ethanol decomposition.

Mass-spectrometry analysis of the desorbed products of ethanol transformation at SnO_2 confirms the course of alcohol decomposition through predominantly the dehydrogenation in a wide range of temperatures (50–400 °C). Thus, the concentration of acetaldehyde (CH_3CHO) in the desorbed products exceeds ethylene (C_2H_4) content more than 10 times.

From the evidence reported one can conclude that the main process determining the efficiency of alcohol detection using semiconducting oxides is oxidising dehydrogenation steps; dehydration have minor significance only. This point should be taken in consideration when selecting advanced gas-sensitive composites for efficient alcohol detection.

Table 4
The comparison of oxide catalytic ability in isopropyl alcohol decomposition process

Oxide	Reactivity ($\ln K$)	
	Dehydrogenation	Dehydration
MoO_3	1.91	0.50
In_2O_3	1.54	0.82
Fe_2O_3	1.52	0.72
SnO_2	1.01	0.44

4. Conclusions

Fe_2O_3 – In_2O_3 based thin films are found to be selective and highly sensitive to alcohol vapour at moderate (300 °C) operating temperature. It was found that the composites, consisted of two contacting phases (In_2O_3 and Fe_2O_3) with large phase interface are preferable materials for gas sensing. In particular, γ - Fe_2O_3 – In_2O_3 (1:1)/ In_2O_3 sensor has the highest dispersity and the most developed phase interface among the Fe_2O_3 – In_2O_3 composites and it is characterised by the best functional parameters. The most sensitive materials consist of two layers. In this case, the specific hetero-junction is forming providing the differentiation between receptor and transducer functions, that improves sensor performance.

It has also been established that the detection of alcohols by using active layers based on investigated oxides is mainly going on the way of oxidising dehydrogenation.

Acknowledgements

This work has been performed in the frame of the EC Programs “INCO-COPERNICUS-II” (GASMOH Project #ICA2-CT-2000-10041) and “INTAS” (Project #2000-0066).

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375 Biographies

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Guido Faglia received an MSc degree from the Polytechnic of Milan in
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and the tin oxide surface and in sensor electrical characterization. In 1996
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Paolo Nelli received his MSc degree in physics from the University of
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semiconducting metal oxides. He is co-author of about 40 papers on
gas sensors and material science and 30 presentations at international
congresses on the same topics.

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